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54 **Reactive hot melt structural adhesive.**

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Description

FIELD OF THE INVENTION

5 The invention relates to reactive hot melt compositions (RHM's) useful as adhesives, sealants, coatings, or the like.

DESCRIPTION OF THE PRIOR ART

10 RHM's are thermosetting adhesives. These materials are known in the prior art, and are known to have various disadvantages.

Canadian Patent 1,229,192 of November 10, 1987, to S.C. Lin, describes an RHM comprising an epoxy urethane containing compound, which thermosets on heating.

15 U.S. 3,723,568 teaches the use of polyepoxides and optional epoxy polymerization catalysts. U.S. 4,122,073 teaches thermosetting resin obtained from polyisocyanates, polyanhydrides and polyepoxides. Crosslinking in these patents is achieved by reaction with available sites in the base polymers. U.S. 4,137,364 teaches crosslinking of an ethylene/vinyl acetate/vinyl alcohol terpolymer using isophthaloyl, bis-caprolactam or vinyl triethoxy silane whereby crosslinking is achieved before heat activation with additional crosslinking induced by heat after application of the adhesive. U.S. 4,116,937 teaches a further method of
20 thermal crosslinking by the use of polyamino bis-maleimide class of flexible polyimides, which compounds can be hot melt extruded up to 150 °C and undergo crosslinking at elevated temperatures thereabove. In these latter two patents, thermal crosslinking is also achieved by reactions of the particular crosslinking agent with available sites of the base polymers.

25 U.S. 3,505,283 teaches the use of simple, organic di- and polyisocyanates as chemical thickeners when reacted with hydroxyl-containing epoxy resins at temperatures between 50 and about 200 °C in the presence of carboxylic acid anhydride as a curing agent. Material prepared from this process is not suitable as a reactive, hot melt adhesive since the high application temperatures required to afford processability may trigger the crosslinking reaction of the thermosetting material prematurely. Similarly, U.S. 3,424,719 teaches the use of simple diisocyanates to react with the glycidyl polyether of dihydric phenols in solvents,
30 thereby increasing the crosslinking density which results in improved heat distortion temperatures. The solvent is necessary for processability of the solid forms of glycidyl polyether dihydric phenol and avoid the high temperature conditions required for polymerization which creates not only process problems but also may induce instability of the reactant mixture after blending with a latent curing agent.

35 OBJECTS OF THE INVENTION

Strong structural adhesives and sealants are needed for bonding substrates loaded with significant mechanical stress at the interface. Such adhesive materials must have the following requirements:

- 40 High production rates with short, unvarying times for each operation in assembly line use.
- Minimal prior cleaning of surfaces to be bonded.
- Minimal health and safety hazards.
- Optimum balance between open time and development of handling strength.
- Maximum bond strength.
- Maximum thermal and environmental resistance.

45 Based on these requirements, typically thermosetting materials such as epoxy resins, phenolics, polyesters, and polyurethanes are used as structural adhesives. After the crosslinking reaction the adhesive becomes part of the structural component and provides the required bond strength and thermal resistance. Normally, the structural adhesive is composed of liquid resins and curing agents in either two-package or single package form depending on the reactivity between the resin and the curing agent under storage
50 conditions.

The liquid structural adhesive has the advantage of easy application to the substrate over the solid adhesive. However, the liquid adhesive, in two-package form after mixing, has a certain length of pot-life which is the time required to stay as liquid for application purposes. Consequently, the handling strength (minimum strength necessary to maintain adhering substrates together) cannot be rapidly developed.
55 Further, from a safety and health hazard viewpoint, the liquid adhesive usually causes more contamination of the work place than the solid form. Thus, the two-package structural adhesive requires a very precise measurement and extremely good mixing to obtain any consistency of property control.

The one package liquid adhesive was designed to solve mixing and metering difficulties. To achieve one package reactive adhesive preparation, techniques such as chemical blocking and phase separation are being used in the adhesive industry. The crosslinking reaction has to be triggered by heating or other techniques which are difficult to control resulting in long time periods to develop handling strength.

5 Two forms of solid adhesives, powder and hot melt can be used instead of liquid adhesives. Because of the phase separation between resin powder and curing agent powder, the one package adhesive can be obtained very easily. However, the application, handling cost and safety considerations make the powder adhesive less attractive to the adhesive industry.

10 The other solid form of adhesive is hot melt which is a thermoplastic in general. The hot melt adhesive provides a bond between substrates upon cooling the molten adhesive to room temperature. The bonding process is fast and simple. The disadvantage of a thermoplastic hot melt adhesive is the fast decrease in its bonding strength upon reheating because of the nature of thermoplastics. Thus, it cannot be considered as a structural adhesive unless it is further modified.

15 Conventional solid adhesive such as high molecular weight epoxy resin can be applied as a reactive hot melt adhesive. Without modification, this type of solid adhesive provides poor adhesion properties such as impact resistance and lap shear strength. Modification of this material such as reacting it with a carboxyl-terminated poly(butadiene-co-acrylonitrile) increases the impact resistance and the lap shear strength. However, this modification is carried out at elevated temperature, 100 - 150 °C, in the presence of a catalyst, thus making the addition of a latent curing agent such as dicyandiamide and curing accelerator 20 difficult since the curing reaction is activated by the catalyst at room temperature. Hence, due to the combination of a high cost factor and preparation difficulties, this type of adhesive is not attractive commercially.

This invention is concerned with the development of a class of reactive hot melt adhesives which will provide rapid development of handling strength and, also, maximum bond strength and thermal resistance 25 as thermosetting adhesives. This invention also relates to a process to utilize the reaction between diisocyanates and hydroxyl groups of the diol and epoxy resin to prepare the reactive hot melt adhesives having latent curability, long storage life, internally modified adhesion properties and well controlled application rheology. The materials for the preparation of this particular reactive hot melt adhesive include a polyisocyanate, a hydroxyl-containing epoxy resin for introducing reactive pendent groups and a diol, 30 preferably a difunctional primary alcohol, for improving the physical properties and for reducing the viscosity of the bulk polymerization medium. Optionally, a reactive plasticizer for reducing the viscosity of bulk polymerization and adjusting the application temperature can be added to the system.

One object of the instant invention is to produce a composition, usable as an adhesive, sealant or coating, which is solventless. Another object of the invention is to produce a composition which can be 35 applied as a hot melt. Still another object of the instant invention is to produce a composition which is heat curable in a minimum time period. A further object of the invention is to produce a novel compound which in combination with a heat reactive epoxy curing agent will result in a thermoset coating, adhesive or sealant on heating. Yet another object of the invention is to produce a thermoplastic composition which can be applied as a hot melt and thereafter cured by a thermally triggered initiator to a thermoset adhesive, 40 sealant or coating at a more elevated temperature. A further object of the instant invention is to produce one or more methods for making a thermoplastic composition which can be applied as a hot melt. Other objects will become apparent from a reading hereinafter.

DESCRIPTION OF THE INVENTION

45 My RHM composition is an improvement in the single-package epoxy RHM adhesive where the composition contains the hardener or catalyst, which is dormant until heat-triggered, whereupon the composition then crosslinks and thermosets. The improvement is several fold, as compared with various commercial single-package RHM adhesives presently used in the auto industry, viz.:

50

55

	Composition I (This invention)	Composition X ⁽¹⁾
Shear strength ⁽²⁾ , MPa (psi)	20.7 (3000)	12.4 (1800)
Peel strength ⁽³⁾ , N/cm (pli)	78.8 - 87.6 (45 - 50)	0 (0)
Impact strength ⁽⁴⁾ , cm kg (" lbs)	69.2 (60)	11.5 (10)
Green tack to oily metal	30 sec.	30 sec.

(1) A single-package RHM adhesive used for auto door hemflanging, in current commercial use.

(2) Shear strength by ASTM D1002.

(3) Peel strength by ASTM D1876, modified by pulling at 12.7 mm/min (0.5 "/min).

(4) Impact strength (1.6 mm (0.062) cold rolled steel, by General Motors test method.

15 DEFINITIONS

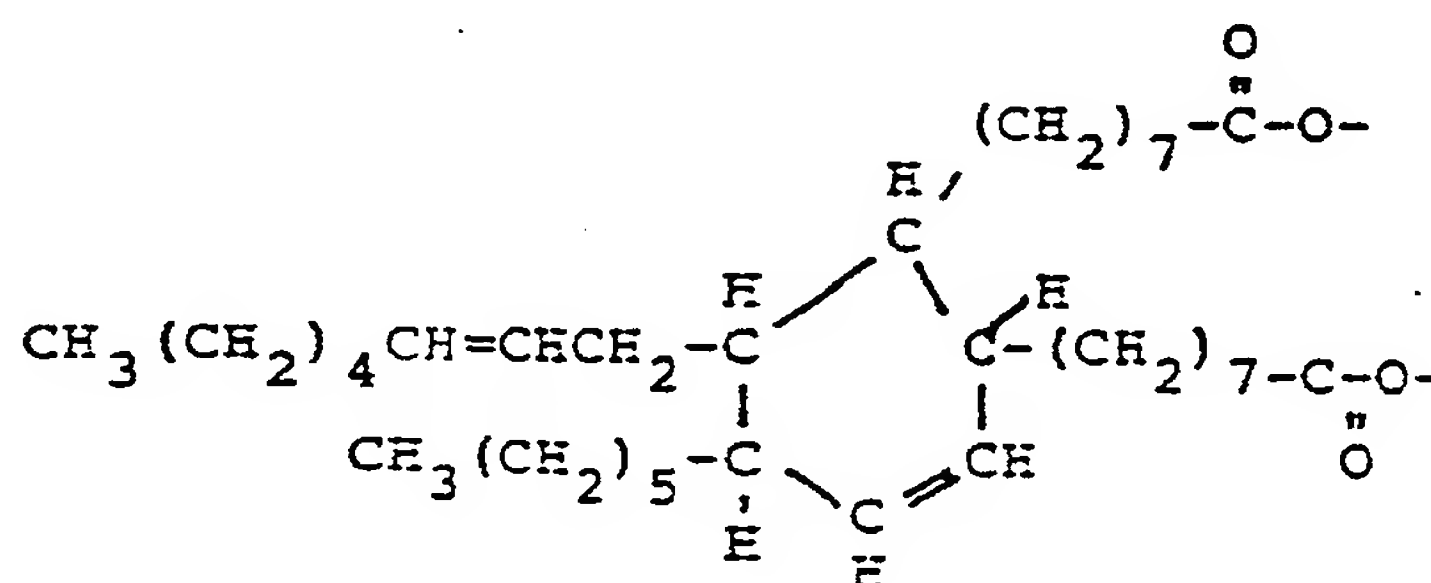
Epoxy resins

Those used in the invention are so-called DGEBA-type, i.e., reaction products of diglycidyl epoxide with Bis-phenol A. All are commercially available from Shell Chemical Co.

Epon-872® has the formula



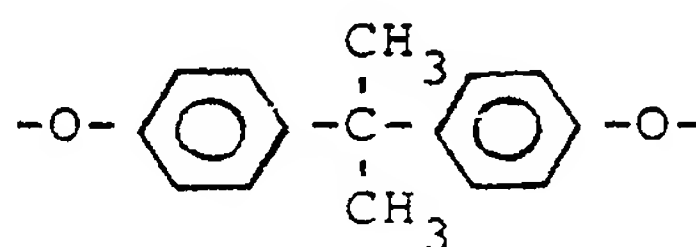
where X is



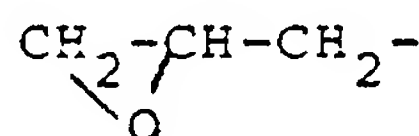
Y is -R-K-Q

where R is -CH₂CH(OH)CH₂-

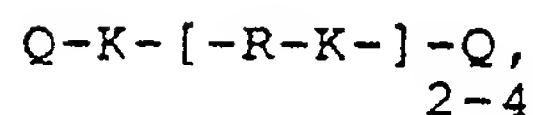
K is



Q is



Epon-1001® F is



with 2.2 -OH groups/molecule

Epon-828® is Q-K-Q, with 0.2 -OH groups/molecule, average MW, 350 - 400.

Other materials

NYAD-400®; calcium silicate powder, from Nyco Co.

N-70-TS®; fumed silica powder, from Cabot Co.

CK-2500®; a non-heat reactive high melting phenolic resin from Union Carbide Corp. Softening point 112.8-143.3 °C (235-290 °F).

A-187®; gamma-Glycidoxypropyltrimethoxy silane, from Union Carbide Corp.

Olin 55-28® is a 4000 g/mole ethylene oxide end-capped polypropylene glycol triblock polymer, with primary hydroxyl groups: ---EO---PO---EO---.

Olin 20-28® is a 4000 g/mole polypropylene glycol homopolymer with secondary hydroxyl groups.

MP-102® (BASF) is a prepolymer made by adding tripropylene glycol to MDI to make a 50:50 MDI:MDI adduct which is liquid at room temperature.

Premix A

Components	Parts by Weight		
	Broad Range	Narrow Range	Specific
Olin 55-28®	5-100	20-25	22.80
Olin 20-28® (1)	0-50	20-25	22.80
Phenyldiethanolamine (2)	0- 2	0- 1	0.47
MP-102® (3)	5-20	5- 9	6.97
Epon-1001F®	0-50	15-20	18.82
Epon-872®	10-50	26-30	28.14

⁽¹⁾When the amount is zero, a more moisture sensitive compound is made.

⁽²⁾When the amount is zero, a softer polymer is made.

⁽³⁾Amount of MP-102® selected such that the ratio of molecular NCO to polyol -OH is greater than 1 but less than 2.

Premix A is a urethane oligomer and is used in TABLE I in the above specific amounts in preparing Composition I. It can be used in modifications of Composition I within the above ranges.

In preparing Composition I (TABLE I), the order of mixing is not critical. However, I prefer to add the dicyandiamide last, with mixing for a short time, to prolong shelf life.

TABLE I

Composition I			
	Parts by Weight		
	Broad Range	Narrow Range	Specific
Premix A	50-800	100-300	250
Epoxy mixture ⁽¹⁾	10-500	50-400	200
Epon-828®	10-200	25-125	50
CaSiO ₃	0-200	50-150	100
CaO	10-100	25- 75	50
Fumed SiO ₂	5- 80	20- 60	40
CK-2500 Phenolic resin	0-100	15- 75	20
Zn ₃ (PO ₄) ₂	5-100	5- 50	10
Dicy/Epoxy mix ⁽²⁾	50-150	60-120	80
gamma-Glycidoxypyrtrimethoxy silane	1- 10	3- 7	5

⁽¹⁾Epon-872®, Epon-1001F®, 3:1.

⁽²⁾Epon-828®/dicyandiamide, 2:1.

When reference is made to Composition I, it is the Composition with the Specific amounts in TABLE I unless otherwise noted. Such Composition is preferred for use herein.

Example 1

This example is partially hypothetical in that it is based on properties of my Composition I that I have established in the laboratory. Composition I use is demonstrated on a section of an auto assembly line, viz., an adhesive/sealant for door hem flange binding.

(1) Composition I at room temperature is a viscous liquid (a semi-solid). For application it must be heated, e.g., to 80 °C, to liquefy it. At 80 °C it has zero strength and is easily handled. This temperature is too low to trigger the curing mechanism. Composition I at about 80 °C is applied around the interior rim of the outer plate (cold rolled steel - "CRS", optionally galvanized) of a car door. This application is preferably by spraying, but it can be by melt extrusion or other system.

(2) The inner plate (CRS) is now pressed ("fixtured") against the outer plate. One or both parts may be oily. In such case Composition I quickly penetrates the oil and forms an adhesive bond to the part. At this stage (room temperature) the Composition provides a strength of about 0.07 MPa (10 psi), enough to hold the two plates together under non-stress conditions.

(3) The flanges of the outer plate are now folded over the perimeter of the inner plate. In this operation, Composition I is squeezed into the flange crevices, providing a good seal all around the perimeter. The strength of the green adhesive at this stage is still about 0.07 MPa (10 psi).

(4) The door is assembled onto the metal body of the car. Here, if need be, the door can be bent and twisted to fit the automobile. If the adhesive bond is broken, possible sites for corrosion are not made because the adhesive softens in Step 6. At this stage the door is dimensionally stable because of the viscosity of the Composition (about 0.07 MPa (10 psi)).

(5) The assembled car body is dipped into E-coat primer bath (a room-size vat). At this point many commercial adhesives tend to dissolve or be partially washed off into the primer baths and to redeposit on the car body surfaces. Composition I does not dissolve in these baths and hence avoids this problem. In this operation, Composition I has a strength of about 0.07 MPa (10 psi).

(6) The assembled body is removed from the E-bath and taken to the baking oven, where it is heated to about 177 °C (350 °F). Composition I at first melts and passes again through zero strength, then quickly begins to cure and soon attains its maximum strength, taking about thirty minutes for this. In its molten condition it spreads further into all cracks and crevices and ensures thorough coating and sealing between the two door plates, thereby minimizing future vapor/liquid penetration between the plates and consequent corrosion. A modification of Step 6 is discussed later on when I describe my Composition II.

The process outlined above has a general applicability. The substrates (adherends) are suitably metal parts. Parts such as refrigerator doors, stove and oven doors, parts for washers and driers, double-walled panels for vans and trucks, and hardware for marine, air, and rail vehicles and accessories can be

assembled by my process, using the compositions of this invention. The invention compositions can also be used as gaskets and sealants.

Referring now back to Stage (4) above, at this point parts adhered with conventional adhesives are customarily visually inspected. Frequently the parts will be very slightly out of true with respect to each other and/or to the car body framework. Manual adjustments (pounding, pulling, pressure) are made at this stage to bring the elements back into true. In current practice, using commercially available structural adhesives, this type of forcible adjustment tends to produce minute cracks in the adhesive, which is a semi-solid at this stage in the process (i.e., after application but before curing). Such cracks presage corrosion and eventual bond-failure. It would be a great advantage if the adhesive could momentarily cease to be a viscous solid and become a liquid with zero strength. My Composition I will in fact do exactly that. Thus, at 100 - 160 °C Composition I melts but does not cure. Above 160 °C it cures. Thus, when heating to 180 °C, the Composition must pass through 100 - 160 °C, so it softens.

This behavior provides a "window" within the process program which permits adjustments, and within which complete assemblies can be structured and/or restructured (i.e., the adherends can be moved with respect to each other). At temperatures below this window my Composition I is a semi-solid or viscous liquid, with very low adhesive strength (ca. 0.07 MPa (10 psi)). At the window, the strength is zero. At temperatures substantially above the window temperature, Composition I will cure, solidify, and develop maximum strength.

Composition II

For assembly lines where Stage (6) above requires something between zero strength and a small but useful strength (e.g., 0.07 MPa (10 psi)), I modify Composition I to Composition II. Composition II is like Composition I in that it is sufficiently liquid to withstand minor adherend adjustments without rupture or development of cracks. On the other hand, it is sufficiently viscous to provide a strength of about 7 kPa (1 psi) at the curing temperature (177 °C), which is helpful in maintaining dimensional stability of the bonded adherends, especially where the Composition is affixed around the entire perimeter of the door or like part. Like Composition I, Composition II can be used to provide two metal substrates having between them the respective composition in uncured molten condition at a temperature of about 80-150 °C.

Composition II is a moisture-curing RHM adhesive, and is described below.

TABLE II

Composition II			
	Parts by Weight		
	Broad Range	Narrow Range	Specific
Premix A	200-1000	400-600	500
CKOO36 Phenolic ⁽¹⁾	5-50	10-30	18.5
CaCO ₃ powder	0-200	50-150	111
Fumed Silica	0-50	15-25	22.2
Dicy/Epoxy Mix ⁽²⁾	5-50	15-25	22.2
Schiff base ⁽³⁾	5-50	15-25	22.2
gamma-Glycidoxypyrtrimethoxy silane	1-10	1-5	3

(1) A non-heat reactive high melting phenolic resin from Union Carbide Corp., with a softening point of about 87.8-112.8 °C (190-235 °F).

(2) Epon-828®/dicyandiamide wt. ratio: 2:1

(3) The Schiff base reacts with atmospheric moisture to regenerate the component amine and aldehyde or Ketone. The amine then catalyzes the cure. Substantially any Schiff base is suitable. The adduct of methyl isobutyl ketone and ethylene diamine is useful and cheap, and is available from Shell Chemical Co. as "H-2" (trademark).

The specific formulation in Table II gave a shear strength of 5.5 MPa (800 psi) and peel strength of 17.5 N/cm (10 pli), by ASTM procedures, *supra*.

The two Compositions (I and II) described in Tables I and II are species of the broader genus set forth in Table III.

TABLE III

Reactive Hot Melt Adhesives	
Component	Parts by Weight
Premix A	50 - 1000
Epon-872®/Epon-1001F®, 3:1	10 - 500
Epon 828®	10 - 200
Calcium Silicate (1)	0 - 200
CaO (2)	0 - 100
Fumed silica (1)	0 - 80
Phenolic resin	5 - 100
Zn ₃ (PO ₄) ₂	5 - 100
Epon-828®/dicyandiamide, 2:1	5 - 150
gamma-Glycidoxypropyltrimethoxy silane	1 - 10
Schiff base (2)	0 - 50
Calcium carbonate powder (1)	0 - 200

(1) Provided that the total of calcium silicate, fumed silica, and calcium carbonate is in the range of about 10-30 (preferably about 20) weight % of the total composition. The amount of fillers is needed to modify the rheology of the liquid mixture and to reinforce the cured product.

(2) When Schiff base is present, CaO is zero, and vice versa. CaO is present to remove all moisture in the composition, whereas Schiff base reacts with atmospheric moisture to regenerate component amine (which is a catalyst) and ketone or aldehyde.

Variations

The use of Epon-1001 F® is not critical. Various other Epons are useful, e.g., Epon-836®, which is: a Bis-phenol A adduct with Epon 828®, viz., QKRKQ, where Q, K, and R are as above defined.

Celanese-5132® (a trimer acid adduct) may be used in whole or in part for Epon-872® (though I prefer the latter).

Substantially any polyisocyanate can be used, substituting in whole or in part for MDI, viz.:

Diisocyanates such as hexamethylene diisocyanate, m-phenylene diisocyanate, 2,4-toluene diisocyanate, 4,4'-diphenylmethane diisocyanate, dianisidine diisocyanate, tolidine isocyanate, isophorone diisocyanate, 4,4'-dicyclohexylmethane, chlorophenylene-2,4-diisocyanate, 1,5-naphthalene diisocyanate, ethylene diisocyanate, diethylidene diisocyanate, propylene-1,2-diisocyanate, cyclohexylene-1,2-diisocyanate, 3,3'-dimethyl-4,4'-biphenylene diisocyanate, 3,3'-dimethoxy-4,4'-biphenylene diisocyanate, 3,3'-diphenyl-4,4'-biphenylene diisocyanate, 4,4'-biphenylene diisocyanate, 3,3'-dichloro-4,4'-biphenylene diisocyanate, and furfurylidene diisocyanate.

Triisocyanates such as biuret of hexamethylene diisocyanate and triphenylmethane triisocyanate.

Polyisocyanates such as polymeric diphenylmethane diisocyanate.

Heating

The heating step to cure my epoxy, urethane-containing, hot melt adhesive compounds to thermoset materials is usually carried out for a period of 10 seconds to 30 minutes at a temperature of 100 - 300 °C, preferably 150 - 200 °C, which is sufficient to fully cure the composition to a solid thermoset adhesive, coating or sealant.

The heating step to cure the compound can be accomplished in several ways. In simple adhesive systems, the composition can be applied by manual means to an adherend, contacted with another adherend and the assembled systems heated in a forced air oven until a thermoset bond results.

The composition according to the invention is defined as follows :

A reactive hot melt composition obtainable by mixing, in parts by weight

(1) Premix A, 50 - 1000 parts;

EP 0 343 676 B1

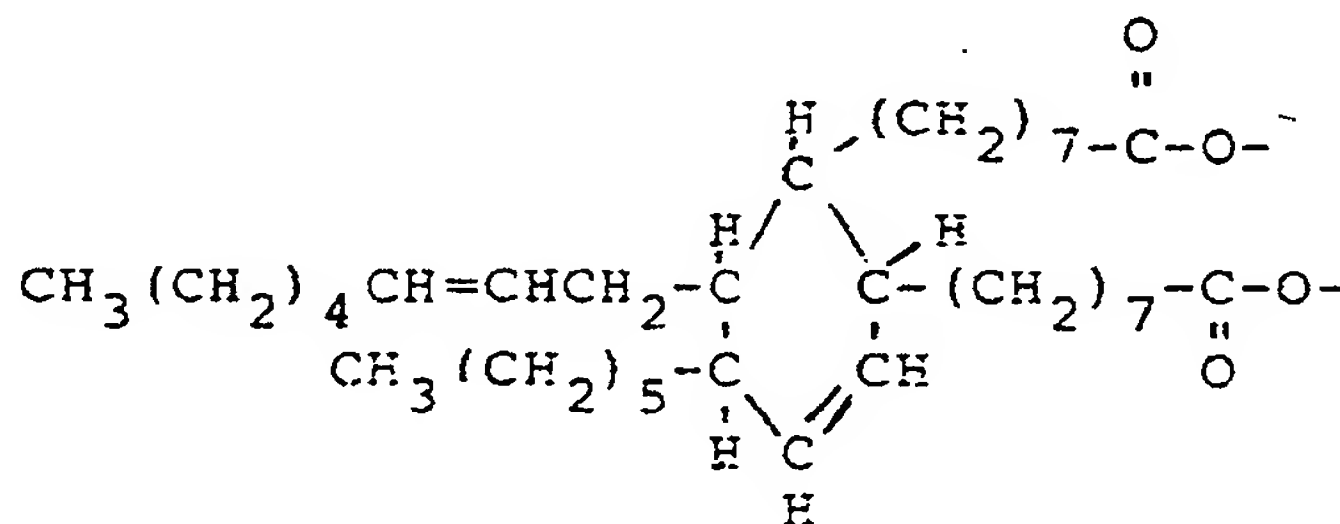
- (2) Epoxy resin mixture consisting of epoxy resin B and epoxy resin C in a weight ratio of about 3:1, 10 - 500 parts;
- (3) Epoxy resin D, 10 - 200 parts;
- (4) Calcium silicate powder, 0 - 200 parts;
- 5 (5) CaO, 0 - 100 parts;
- (6) Fumed silica, 0 - 80 parts;
- (7) Phenolic resin, softening point 87.8 - 143.3 °C (190 - 290 °F), non-heat reactive, 5 - 100 parts;
- (8) $Zn_3(PO_4)_2$, 5 - 100 parts;
- (9) Mixture, about 2:1 by weight, of Epoxy resin D and dicyandiamide 5 - 150 parts;
- 10 (10) gamma-Glycidoxypopyltrimethoxy silane, 1 - 10 parts;
- (11) Schiff base, 0 - 50 parts; and
- (12) $CaCO_3$ powder, 0- 200 parts;

where Premix A comprises in parts by weight,

- (i) a ca. 4000 g/mole ethylene oxide end-capped polypropylene glycol triblock copolymer, - - - ethylene oxide - - - propylene oxide - - - ethylene oxide - - -, containing primary -OH groups, 5 - 100 parts;
- (ii) a ca. 4000 g/mole polypropylene glycol homopolymer, with secondary -OH groups, 0 - 50 parts;
- (iii) phenyl diethanolamine, 0 - 2 parts;
- (iv) about 50:50 weight mixture of diphenyl-methane diisocyanate and an adduct of tripropylene glycol and diphenyl methane diisocyanate, 5 - 20 parts, wherein diphenyl methane diisocyanate can completely or partly be replaced by other diisocyanates, by triisocyanates or by other polyisocyanates, and wherein the amount of this mixture is further selected such that the molecular ratio of -NCO/polyol -OH is between 1 and 2;
- (v) Epoxy resin C, 0 - 50 parts;
- (vi) Epoxy resin B, 10 - 50 parts.
- where Epoxy resin B is



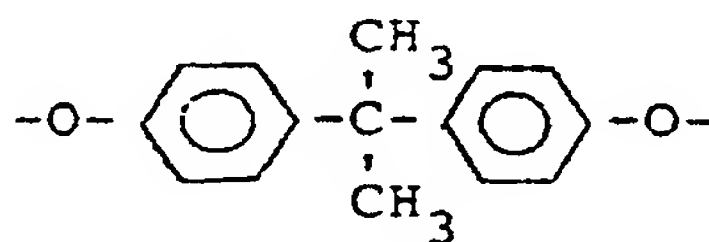
where X is:

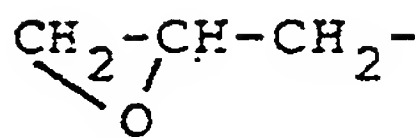


Y is -R-K-Q

R is $-\text{CH}_2\text{CH}(\text{OH})\text{CH}_2-$

K is





5

Epoxy resin C is



Epoxy resin D is Q-K-Q

Provided that, when CaO is present, then Schiff base is zero, and vice-versa; and

15 Provided that the total of calcium silicate, fumed silica, and calcium carbonate is in the range of about 10-30 weight % of the total composition.

Preferred compositions are the following:

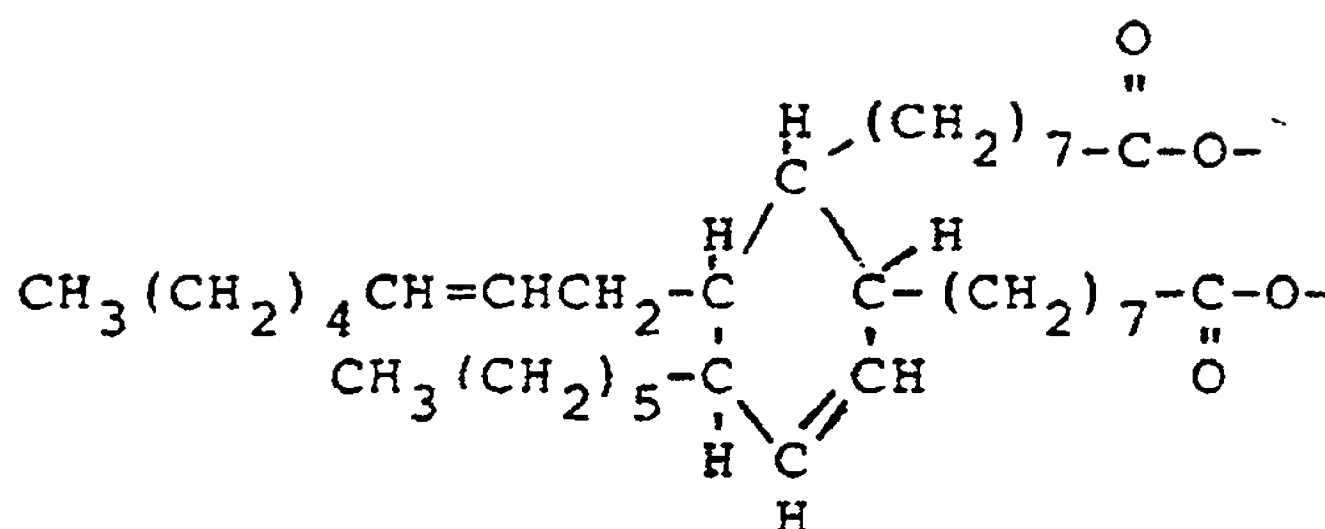
1. A composition wherein, in parts by weight,
 (1) Premix A is 50 - 800 parts;
 (2) The mixture of epoxy resins B and C is 10 - 500 parts;
 (3) Epoxy resin D is 10 - 200 parts;
 (4) Calcium silicate is 0 - 200 parts;
 (5) CaO is 10 - 100 parts;
 (6) Fumed silica is 5 - 80 parts;
 (7) Phenolic resin, softening point 112.8-143.3° C (235-290° F), is 5 - 100 parts;
 (8) $Zn_3(PO_4)_2$ is 5 - 100 parts;
 (9) Epoxy resin D/dicyandiamide mixture is 50 - 150 parts;
 (10) gamma-Glycidoxypyrroltrimethoxy silane is 1 - 10 parts.
 (11) Schiff base, 0; and
 (12) $CaCO_3$ powder, 0.
2. A Composition wherein, in parts by weight,
 (1) Premix A is 50 - 800 parts;
 (2) The mixture of epoxy resins B and C is 50 - 400 parts;
 (3) Epoxy resin D is 25-125 parts;
 (4) Calcium silicate is 50 - 150 parts;
 (5) CaO is 25-75 parts;
 (6) Fumed silica is 20 - 60 parts;
 (7) Phenolic resin is 15 - 75 parts;
 (8) $Zn_3(PO_4)_2$ is 5 - 50 parts;
 (9) Epoxy resin D/dicyandiamide mixture is 60 - 120 parts;
 (10) gamma-Glycidoxypyrroltrimethoxy silane is 3 - 7 parts;
3. A composition wherein, in parts by weight,
 (1) Premix A is 50 - 800 parts;
 (2) The mixture of epoxy resins B and C is 200 parts;
 (3) Epoxy resin D is 50 parts;
 (4) Calcium silicate is 100 parts;
 (5) CaO is 50 parts;
 (6) Fumed silica is 40 parts;
 (7) Phenolic resin is 20 parts;
 (8) $Zn_3(PO_4)_2$ is 10 parts;
 (9) Epoxy resin D/dicyandiamide mixture is 80 parts;
 (10) gamma-Glycidoxypyrroltrimethoxy silane is 5 parts.
4. A composition wherein, in parts by weight, (1) Premix A is 100 - 300 parts.
5. A composition-wherein, in parts by weight, (1) Premix A is 250 parts.
6. A composition consisting essentially of, in parts by weight,
 (1) Premix A, 200-1000 parts;
 (6) Fumed silica, 0-50 parts;
 (7) Phenolic resin, softening point 87.8-112.8° C (190-235° F), 0-50 parts;

- (9) Epoxy resin D/dicyandiamide mixture, 5-50 parts;
 (10) gamma-Glycidoxypropyltrimethoxy silane, 1-10 parts;
 (11) Schiff base, 5-50 parts; and
 (12) Calcium carbonate, 0-200 parts.
- 5 7. A composition wherein, in parts by weight,
 (1) Premix A is 400-600 parts;
 (6) Fumed silica is 15-25 parts;
 (7) Phenolic resin is 10-30 parts;
 (9) Epoxy resin D/dicyandiamide mixture is 15-25 parts;
 10 (10) gamma-Glycidoxypropyltrimethoxy silane is 1-5 parts;
 (11) Schiff base is 15-25 parts; and
 (12) Calcium carbonate is 50-150 parts.
8. A composition wherein, in parts by weight,
 (1) Premix A is 500 parts;
 15 (6) Fumed silica is 22.2 parts;
 (7) Phenolic resin is 18.5 parts;
 (9) Epoxy resin D/dicyandiamide mixture, 22.2 parts;
 (10) gamma-Glycidoxypropyltrimethoxy silane is 3 parts;
 (11) Schiff base is 22.2 parts; and
 20 (12) Calcium carbonate is 111 parts.

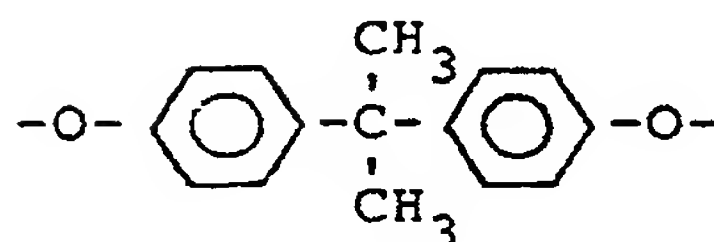
Claims

1. A reactive hot melt composition obtainable by mixing, in parts by weight
- 25 (1) Premix A, 50 - 1000 parts;
 (2) Epoxy resin mixture consisting of epoxy resin B and epoxy resin C in a weight ratio of about 3:1,
 10 - 500 parts;
 (3) Epoxy resin D, 10 - 200 parts;
 (4) Calcium silicate powder, 0 - 200 parts;
 30 (5) CaO, 0 - 100 parts;
 (6) Fumed silica, 0 - 80 parts;
 (7) Phenolic resin, softening point 87.8 - 143.3 ° C (190 - 290 ° F), non-heat reactive, 5 - 100 parts;
 (8) $Zn_3(PO_4)_2$, 5 - 100 parts;
 (9) Mixture, about 2:1 by weight, of Epoxy resin D and dicyandiamide 5 - 150 parts;
 35 (10) gamma-Glycidoxypropyltrimethoxy silane, 1 - 10 parts;
 (11) Schiff base, 0 - 50 parts; and
 (12) $CaCO_3$ powder, 0- 200 parts;
- where Premix A comprises in parts by weight,
 (i) a ca. 4000 g/mole ethylene oxide end-capped polypropylene glycol triblock copolymer, - - -
 40 ethylene oxide - - - propylene oxide - - -ethylene oxide - - -, containing primary -OH groups, 5 - 100
 parts;
 (ii) a ca. 4000 g/mole polypropylene glycol homopolymer, with secondary -OH groups, 0 - 50 parts;
 (iii) phenyl diethanolamine, 0 - 2 parts;
 (iv) about 50:50 weight mixture of diphenyl-methane diisocyanate and an adduct of tripropylene
 45 glycol and diphenyl methane diisocyanate, 5 - 20 parts, wherein diphenyl methane diisocyanate can
 completely or partly be replaced by other diisocyanates, by triisocyanates or by other
 polyisocyanates, and wherein the amount of this mixture is further selected such that the molecular
 ratio of -NCO/polyol -OH is between 1 and 2;
 (v) Epoxy resin C, 0 - 50 parts;
 50 (vi) Epoxy resin B, 10 - 50 parts.
- where Epoxy resin B is

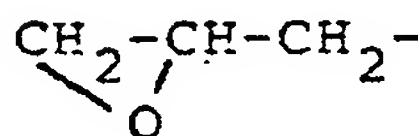




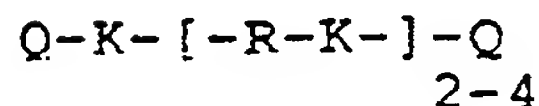
K is



Q is



Epoxy resin C is



Provided that the total of calcium silicate, fumed silica, and calcium carbonate is in the range of about 10-30 weight % of the total composition.

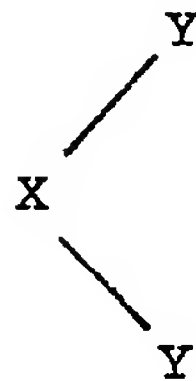
- (10) gamma-Glycidoxypopyltrimethoxy silane is 3 - 7 parts.

- 5. Article comprising two metal substrates containing therebetween the composition of Claims 1 or 2.**

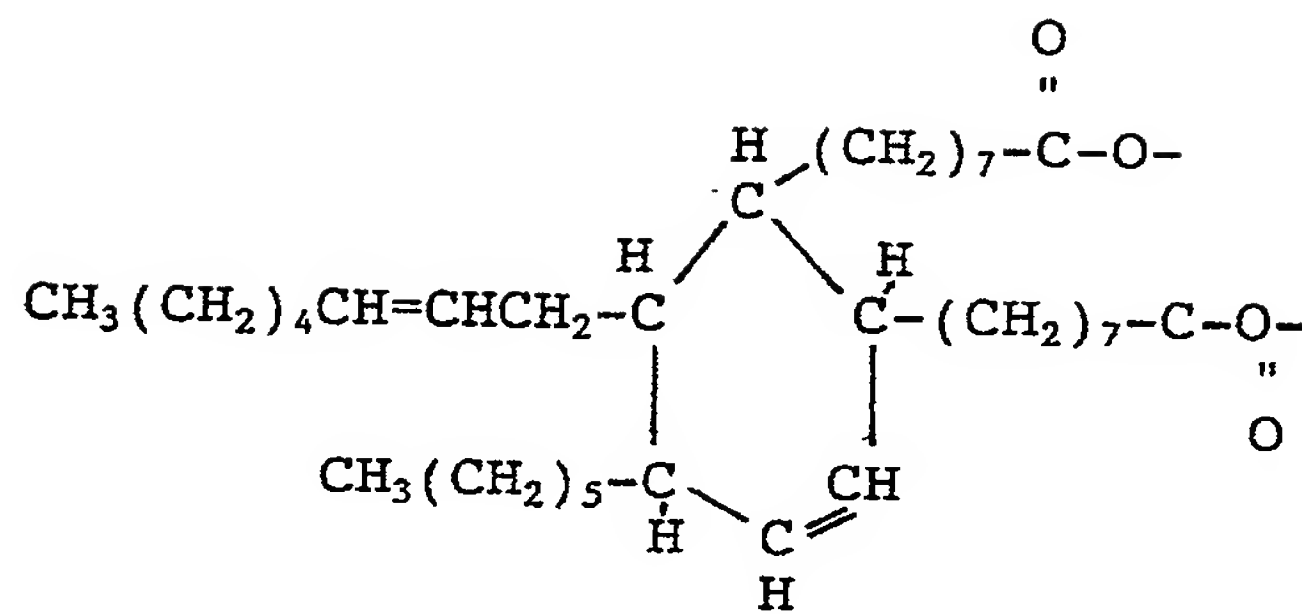
6. Article comprising two metal substrates having therebetween the composition of Claims 1 or 2 in uncured molten condition at a temperature of about 80 - 150 °C.
7. Article comprising 2 metal substrates bonded by having between them uncured molten to semi-molten adhesive composition of Claims 1 or 2, having a shear strength of about 0 to 69 kPa (0 - 10 psi) and a temperature of about 80 - 160 °C; the substrates being movable with respect to each other without loss of bond.
8. Article according to Claim 5, 6 or 7, which is coated.
9. Process of adhering two substrates together comprising the sequential steps of
 - (1) heating the adhesive composition of Claims 1 or 2 to 80 - 140 °C to melt same, but without curing;
 - (2) applying the heated adhesive composition to a metal substrate;
 - (3) fixturing a second metal substrate into intimate contact with the adhesive composition so as to form a bond between the two assembled substrates;
 - (4) heating the bonded substrates at a temperature of 150 - 200 °C to cure the adhesive composition, and to cause adhesion of the substrates.
10. Process according to Claim 9 wherein between steps 3 and 4,
 - 3-a. bonded substrates are integrated into further apparatus, said integration involving stress to the bonded substrates, but without loss of bonding integrity of the composition therein; and
 - 3-b. the further apparatus is coated by exposure to excess coating liquid, without dissolution of the adhesive composition into the coating liquid.

Patentansprüche

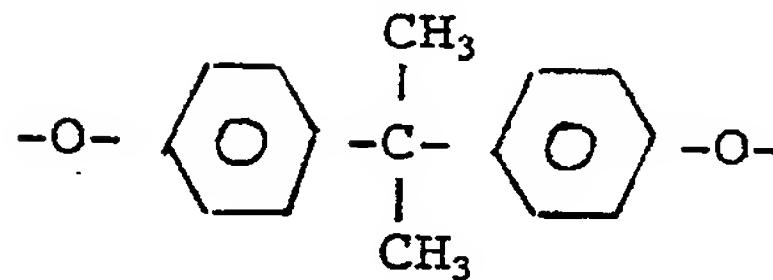
1. Durch Mischen erhältliche reaktive Heißschmelzzusammensetzung, mit in Gewichtsteilen
 - (1) Premix A, 50 - 1000 Teile;
 - (2) Epoxyharzmischung bestehend aus Epoxyharz B und Epoxyharz C in einem Gewichtsverhältnis von etwa 3:1, 10 - 500 Teile;
 - (3) Epoxyharz D, 10 - 200 Teile;
 - (4) Calciumsilikatpulver, 0 - 200 Teile;
 - (5) CaO, 0 - 100 Teile;
 - (6) Quarzstaub, 0 - 80 Teile;
 - (7) Phenolisches Harz, Erweichungspunkt 87,8 - 143,3 °C (190 - 290 °F), nicht wärmereaktiv, 5 - 100 Teile;
 - (8) $Zn_3(PO_4)_2$, 5 - 100 Teile;
 - (9) Mischung von Epoxyharz D und Dicyandiamid, etwa 2:1 bezogen auf das Gewicht, 5 - 150 Teile;
 - (10) γ -Glycidoxypropyltrimethoxysilan, 1 - 10 Teile;
 - (11) Schiffsche Base, 0 - 50 Teile; und
 - (12) $CaCO_3$ -Pulver, 0 - 200 Teile;wobei Premix A in Gewichtsteilen
 - (i) ein ca. 4000 g/Mol Polypropylenglykoltriblock-Copolymer mit Ethylenoxyd-Endgruppen, ---Ethylenoxyd---Propylenoxyd---Ethylenoxyd---, welches primäre OH-Gruppen enthält, 5 - 100 Teile;
 - (ii) ein ca. 4000 g/Mol Polypropylenglykol-Homopolymer mit sekundären OH-Gruppen, 0 - 50 Teile;
 - (iii) Phenyldiethanolamin, 0 - 2 Teile;
 - (iv) eine bezogen auf das Gewicht etwa 50:50-Mischung von Diphenylmethandiisocyanat und einem Addukt von Tripropylenglykol und Diphenylmethandiisocyanat, 5 - 20 Teile, wobei das Diphenylmethandiisocyanat vollständig oder teilweise durch andere Diisocyanate, durch Triisocyanate oder durch andere Polyisocyanate ersetzt sein kann und wobei die Menge dieser Mischung weiter derart ausgewählt ist, daß das molekulare Verhältnis von -NCO/Polyol-OH zwischen 1 und 2 ist;
 - (v) Epoxyharz C, 0 - 50 Teile; und
 - (vi) Epoxyharz B, 10 - 50 Teile, enthält,wobei Epoxyharz B



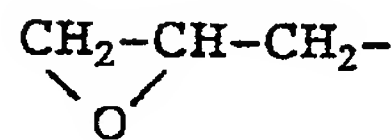
ist, und
wobei X ist



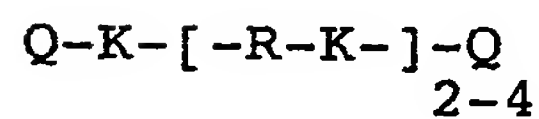
Y ist -R-K-Q
R ist -CH₂CH(OH)CH₂-
K ist



Q ist



Epoxyharz C ist



Epoxyharz D ist Q-K-Q,

vorausgesetzt, daß dann, wenn CaO vorliegt, die Menge an Schiffscher Base Null ist und umgekehrt; und vorausgesetzt, daß die Gesamtmenge an Calciumsilikat, Quarzstaub und Calciumcarbonat im Bereich von etwa 10 - 30 Gew.-%, bezogen auf die gesamte Zusammensetzung, liegt.

EP 0 343 676 B1

2. Zusammensetzung nach Anspruch 1, wobei in Gewichtsteilen
- (1) Premix A in 50 - 800 Teilen;
 - (2) Die Mischung aus Epoxyharzen B und C in 50 - 400 Teilen;
 - (3) Epoxyharz D in 25 - 125 Teilen;
 - 5 (4) Calciumsilikat in 50 - 150 Teilen;
 - (5) CaO in 25 - 75 Teilen;
 - (6) Quarzstaub in 20 - 60 Teilen;
 - (7) Phenolisches Harz in 15 - 75 Teilen;
 - (8) $Zn_3(PO_4)_2$ in 5 - 50 Teilen;
 - 10 (9) Epoxyharz D/Dicyandiamid-Mischung in 60 - 120 Teilen; und
 - (10) γ -Glycidoxypropyltrimethoxysilan in 3 - 7 Teilen vorliegt.
3. Gehärtete Zusammensetzung, die durch Erwärmen der Zusammensetzung nach den Ansprüchen 1 oder 2 auf 100 bis 300 °C hergestellt ist.
- 15 4. Zusammensetzung nach Anspruch 3, die durch Erwärmen auf 150 bis 200 °C hergestellt ist.
5. Gegenstand, welcher zwei Metallsubstrate mit dazwischenliegender Zusammensetzung nach den Ansprüchen 1 oder 2 aufweist.
- 20 6. Gegenstand, welcher zwei Metallsubstrate mit dazwischenliegender Zusammensetzung nach den Ansprüchen 1 oder 2 in ungehärtetem geschmolzenen Zustand bei einer Temperatur von etwa 80 - 150 °C aufweist.
- 25 7. Gegenstand, welcher zwei Metallsubstrate aufweist, die miteinander verbunden sind, indem zwischen ihnen die ungehärtete geschmolzene bis halbggeschmolzene Klebstoffzusammensetzung nach den Ansprüchen 1 oder 2 vorliegt, welche eine Scherfestigkeit von etwa 0 bis 69 kPa (0 - 10 psi) und eine Temperatur von etwa 80 - 160 °C aufweist, wobei die Substrate ohne Auflösung der Bindung relativ zueinander bewegbar sind.
- 30 8. Gegenstand nach den Ansprüchen 5, 6 oder 7, der beschichtet ist.
9. Verfahren zum Zusammenkleben von zwei Substraten, bei dem nacheinander
- (1) die Klebstoffzusammensetzung nach den Ansprüchen 1 oder 2 auf 80 - 140 °C erwärmt wird, um
 - 35 diese ohne Härtung zu schmelzen;
 - (2) die erwärmte Klebstoffzusammensetzung auf ein Metallsubstrat aufgebracht wird;
 - (3) ein zweites Metallsubstrat in engem Kontakt mit der Klebstoffzusammensetzung fixiert wird, so daß eine Bindung zwischen den zwei zusammengefügt Substraten gebildet wird; und
 - (4) die verbundenen Substrate auf eine Temperatur von 150 - 200 °C erwärmt werden, um die
 - 40 Klebstoffzusammensetzung zu härten und ein Aneinanderhaften der Substrate zu bewirken.
10. Verfahren nach Anspruch 9, bei dem zwischen den Schritten 3 und 4
- 3-a. die verbundenen Substrate in eine weitere Vorrichtung integriert werden, wobei die Integrierung zu einer Belastung der verbundenen Substrate führt, aber ohne daß die Unversehrtheit der Bindung
 - 45 der darin befindlichen Zusammensetzung verloren geht; und
 - 3-b. die weitere Vorrichtung durch Behandlung mit überschüssiger Beschichtungsflüssigkeit beschichtet wird, ohne daß sich die Klebstoffzusammensetzung in der Beschichtungsflüssigkeit auflöst.

Revendications

- 50 1. Une composition du type fusion à chaud réactive, que l'on peut obtenir en mélangeant en parties en poids :
- (1) Premix A, 50 - 1000 parties
 - (2) Mélange de résines époxy formé de résine époxy B et de résine epoxy C, dans un rapport
 - 55 pondéral environ de 3:1, 10 - 500 parties
 - (3) Résine D Epoxy 10 - 200 parties
 - (4) Silicate de calcium en poudre 0 - 200 parties
 - (5) CaO, 0 - 100 parties

EP 0 343 676 B1

(6) Fumée de silice 0 - 80 parties

(7) Résine phénolique point de ramollissement 87.8 - 143.3 °C (190 - 290 °F), non réactive à la chaleur 5 - 100 parties

(8) $(\text{PO}_4)_2 \text{Zn}_3$ 5 - 100 parties

5 (9) Mélange environ 2:1 en poids de résine D Epoxy et de dicyandiamide 5 - 150 parties

(10) gamma-glycidoxypropyltriméthoxy silane, 1 - 10 parties

(11) Base de Schiff 0 - 50 parties

(12) CO_3Ca en poudre 0 - 200 parties

dans lequel Premix A comprend en parties en poids

10 (i) un homopolymère d'environ 4000 g/mole environ de polypropylène glycol triblock copolymère - à extrémité couverte par un oxyde d'éthylène - - éthylène oxyde - - - propylène oxyde - - - éthylène oxyde - - -, contenant des groupes -OH primaires 5 - 100 parties

(ii) un homopolymère d'environ 4000 g/mole de polypropylène glycol ayant des groupes -OH secondaires, 0 - 50 parties

15 (iii) phényl diéthanolaamine, 0 - 2 parties.

(IV) un mélange environ 50:50 en poids de diphénylméthane diisocyanate et d'un produit d'addition de tripropylèneglycol et de diphénylméthane diisocyanate 5 à 20 parties dans lequel le diphénylméthane diisocyanate peut être complètement ou partiellement remplacé par d'autres isocyanates et dans lequel la quantité de ce mélange est en outre choisie de telle sorte que le rapport moléculaire de -NCO/OH de polyol est compris entre 1 et 2.

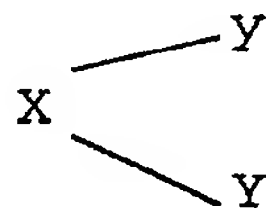
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V) résine époxy C 0 - 50 parties

VI) résine époxy B 10 - 50 parties

dans laquelle la résine époxy B est :

25



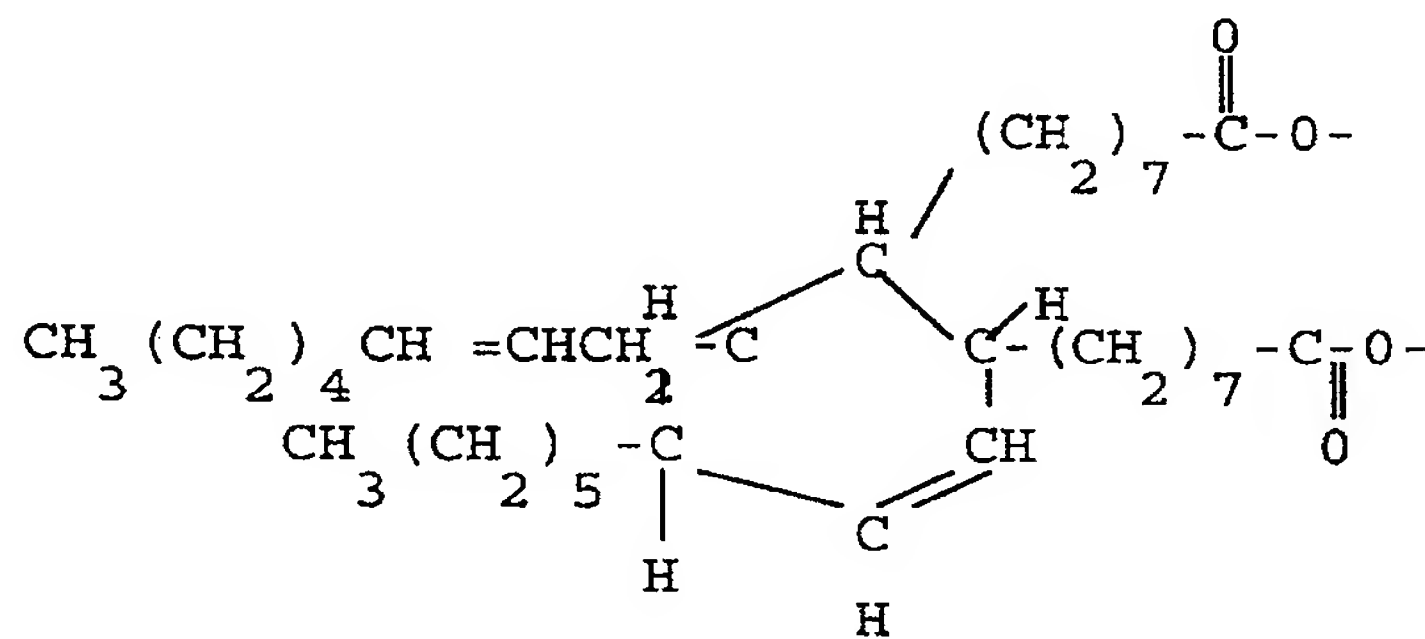
30

ou X est :

35

40

45



Y est -R-K-Q

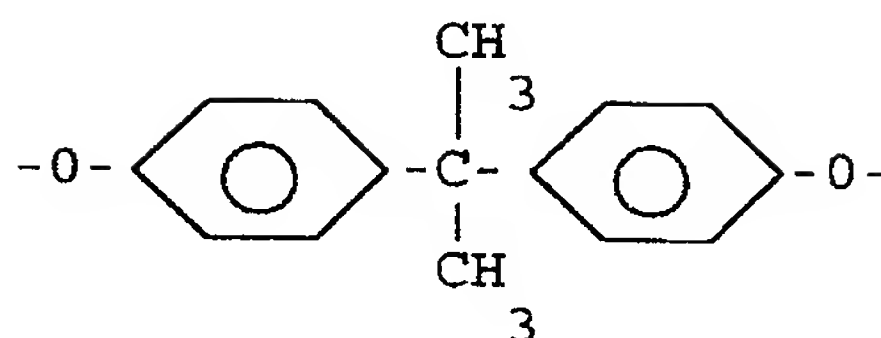
dans laquelle

50

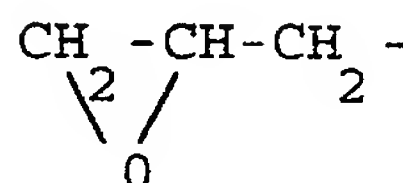
R est $-\text{CH}_2\text{CH}(\text{OH})\text{CH}_2-$

K est

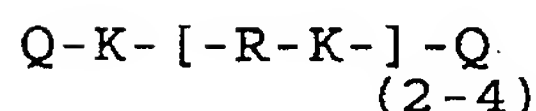
55



Q est



La résine Epoxy C est



La résine Epoxy D est Q-K-Q

à la condition que lorsque CaO est présent alors la base de Schiff est zéro et vice et versa, et à la condition que le total silicate de calcium, fumée silice, et le carbonate de calcium est dans la gamme environ de 10 à 30 % en poids de la composition totale.

2. Composition selon la revendication 1 dans laquelle on trouve en parties en poids :

- (1) Premix A, est 50 - 800 parties
- (2) le mélange de résine époxy B et de résine epoxy C est 50 - 400 parties
- (3) Résine D époxy, est 25 - 125 parties
- (4) le silicate de calcium en poudre est 50 - 150 parties
- (5) CaO, est 25 - 75 parties
- (6) la fumée de silice est 20 - 60 parties
- (7) la résine phénolique est 15 - 75 parties
- (8) $(\text{PO}_4)_2 \text{Zn}_3$ 5 - 50 parties
- (9) Mélange d'Epoxy résine D/dicyandiamide est 60 - 120 parties
- (10) gamma-glycidoxypropyltriméthoxy silane, est 3 - 7 parties

3. Composition durcie faite par chauffage de la composition de la revendication 1 ou 2 à 100 à 300 ° C.

4. Composition selon la revendication 3 qui est faite en chauffant à 150 à 200 ° C.

5. Article comprenant deux substrats métalliques contenant entre eux la composition de la revendication 1 ou 2.

6. Article comprenant deux substrats métalliques ayant entre eux la composition selon la revendication 1 ou 2, à l'état fondu non durci à une température d'environ 80 à 150 ° C.

7. Article comprenant deux substrats métalliques reliés en ayant entre eux la composition adhésive non durcie fondue à semi-fondue, de la revendication 1 ou 2, ayant une force de cisaillement environ de 0 à 69 kPa/0-10 psi) et une température environ de 80-160 ° C ; les substrats étant déplaçable par rapport à l'autre sans perte de liaison.

8. Article selon la revendication 5, 6 ou 7 qui est enduit.

9. Procédé pour faire adhérer deux substrats ensemble qui comprend les étapes successives de :

EP 0 343 676 B1

- 1) chauffer la composition adhésive de la revendication 1 ou 2, à 80-140 ° C pour faire fondre celle-ci mais sans la durcir,
- 2) appliquer la composition adhésive chauffée sur un substrat métallique,
- 3) fixer d'une manière inamovible un second substrat métallique en contact intime avec la composition adhésive de façon à former une liaison entre les deux substrats assemblés,
- 4) chauffer les substrats liés à une température de 150 à 200 ° C, pour durcir la composition adhésive et pour provoquer l'adhésion des substrats.

10. Procédé selon la revendication 9 dans lequel entre les étapes 3 et 4.

3a- les substrats liés sont intégrés dans un appareil supplémentaire, la dite intégration impliquant une contrainte pour les substrats reliés mais sans perte de l'intégrité de liaison de la composition à l'intérieur.

3b- l'appareil supplémentaire est enduit par exposition à un liquide d'enduction en excès sans dissolution de la composition adhésive dans le liquide d'enduction.